



# REVISTA AIDIS

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## APPLICABILITY OF THE APPROXIMATE DELTA METHOD FOR DETERMINATION OF THE REAERATION COEFFICIENT IN SUB-BASINS IN THE CENTRAL REGION OF RIO GRANDE DO SUL, BRAZIL

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### Abstract

*The approximate delta method is a simplified experimental method easy to apply and low cost, it is based on the estimated surface reaeration, primary production, and respiration, basically using diurnal measurements of dissolved oxygen (DO). This study aimed to analyze the feasibility of applying this method to determine the reaeration coefficient ( $k_a$ ) in sub-basins of the central region of Rio Grande do Sul. The study was carried out in four sub-basins of the Vacacaí Mirim River, and one sub-basin of the Vacacaí River. In the fluvimetric stations studied, one determined the values of velocity, depth, and flow rate, as well as the DO profile during the photoperiod. In three of the sub-basins, it was not possible to determine the  $k_a$  due to the occurrence of minimum DO deficit before solar noon and/or to the formation of an inappropriate DO profile curve. In the other two sub-basins, it was possible to determine the coefficient, although with some limitations that need to be better investigated since this method is an important alternative to the traditional ones.*

**Keywords:** dissolved oxygen, hydrodynamic characteristics, reaeration coefficient, water quality modeling.

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## Introduction

A chronic problem of Brazilian urban rivers is the quality of its waters. The rivers, historically, are used as drainpipes of the effluents generated by the population. Most of these are not treated or inefficiently treated effluents, which turns the water body unavailable for bathing, supply, and maintenance of aquatic ecosystems (Von Sperling; Von Sperling, 2013). The Brazil Federal law N<sup>o</sup>. 9433, January 1997 (Brasil, 1997), known as the Water Law, outlined a process for managing this vital resource for life support and allowed national and state councils to establish management tools. An important tool to develop management and planning measures of water resources in river basins are the models of water quality (Panagopoulos *et al.*, 2012), which has been widely used to assist water resource managers in planning and decision-making (Silva *et al.*, 2017; Gomes *et al.*, 2018; Lima *et al.*, 2018; Wrublack *et al.*, 2018; Kuchinski; Gastaldini, 2018).

The dissolved oxygen (DO) balance is essential in mathematical models of water quality based on self-depuration, such as Streeter-Phelps model (Streeter; Phelps, 1925), QUAL2E (Wang *et al.*, 2017), QUAL2K (Rehana; Dhanya, 2018), QUAL-UFMG (Gomes *et al.*, 2018; Lima *et al.*, 2018), SAD-IPH (Silva *et al.*, 2017), among others, in which the DO production is estimated by the reaeration coefficient ( $k_a$ ) (Matos *et al.*, 2011). Empirical models or experimental methods can determine the  $k_a$ . Experimental methods, such as the gas tracer (Rathbun; Grant, 1978), soluble probe (Giorgetti; Schulz, 1990) and sound pressure (Morse *et al.*, 2007), require collections of samples, laboratory analyzes, and analysis of data, making the determination of the  $k_a$  an expensive and time-consuming task, which demand a large work team (Gonçalves *et al.*, 2017; Queiroz *et al.*, 2015). The tracer method is one of the most accurate to determine the  $k_a$ ; however, it requires a specialized team, acquisition of materials, and the costs of field and laboratory analyzes are significant, leading to restrictions in its use (Costa *et al.*, 2015; Soares *et al.*, 2013). This becomes evident in the study carried out by Formentini (2010) in Vacacaí Mirim basin, who performed only two experiments using this method.

For this reason, empirical models are employed in studies to determine the  $k_a$ , such as O'Connor and Dobbins (1958), Churchill *et al.* (1962), Elmore and Buckingham (1962), Owens Edwards and Gibbs (1964), Tsivoglou and Wallace (1972), Parker and Gay (1987), Smoot (1988), Melching and Flores (1999), Jha *et al.*, (2001), Ojha and Bhatia, K.K.S (2001). These models are based on considerations of theoretical mass transfer and statistical correlation values of  $k_a$  with hydrodynamic characteristics, and they consist of equations that require the hydrodynamic characteristics of the river (Palumbo *et al.*, 2014). However, when using these equations to calculate the  $k_a$  in different locations from where they were drawn up, one can insert uncertainties in the process, since they are more accurate to the location where they were originated from (Queiroz *et al.*, 2015). Therefore, field investigations at the fluvimetric station of interest would be the best way to estimate the  $k_a$  (Haider *et al.*, 2013).

The approximate delta method (ADM) (Mcbride; Chapra, 2005), developed from the delta method (Chapra; Di Toro, 1991), was proposed as a simpler alternative to experimental methods. This method requires few resources to determine the  $k_a$ , as a DO meter and meteorological data. Although the proposal is apparently easy to apply, it has not yet been widely used. Since the method is a low cost alternative applied in loco, the objective of this study is to analyze the feasibility of applying the ADM to determine the  $k_a$ , and understand why this method is not widely used. We applied the ADM in five sub-basins of the central region of Rio Grande do Sul, Brazil.

The technical note is organized in four Sections. Section 2 introduces the ADM to determine the  $k_a$ . Section 3 presents the applications of the method in five urban sub-basins in the central region of Rio Grande do Sul, and finally, Section 4 exposes the considerations and conclusions of the study.

### Approximate delta method

The ADM can be defined as a simple procedure for the simultaneous calculation of  $k_a$ , primary production rate, and respiration rate in a river stretch using the DO diurnal profile. This curve indicates that both the minimum and maximum concentration of DO occur during the photoperiod, the first between sunrise and solar noon, and the second between solar noon (SN) and sunset, considering the appropriate DO profile (Mcbride; Chapra, 2005). We shall detail only the equations to determine the  $k_a$ , aimed of this study. More details about the method are found in McBride and Chapra (2005).

The  $k_a$  ( $\text{days}^{-1}$ ) is determined as a function of the time between the minimum DO deficit (MDOD) and the solar noon, regardless the primary production rate and respiration, given by:

$$k_a = 7.5 \left( \frac{5.3\eta - \Phi}{\eta\Phi} \right)^{0.85} \quad \text{Equation (1)}$$

where,  $\Phi$  (hours) is the time between MDOD and SN, defined as:

$$\Phi = t_{min} - \left( \frac{f}{2} \right) \quad \text{Equation (2)}$$

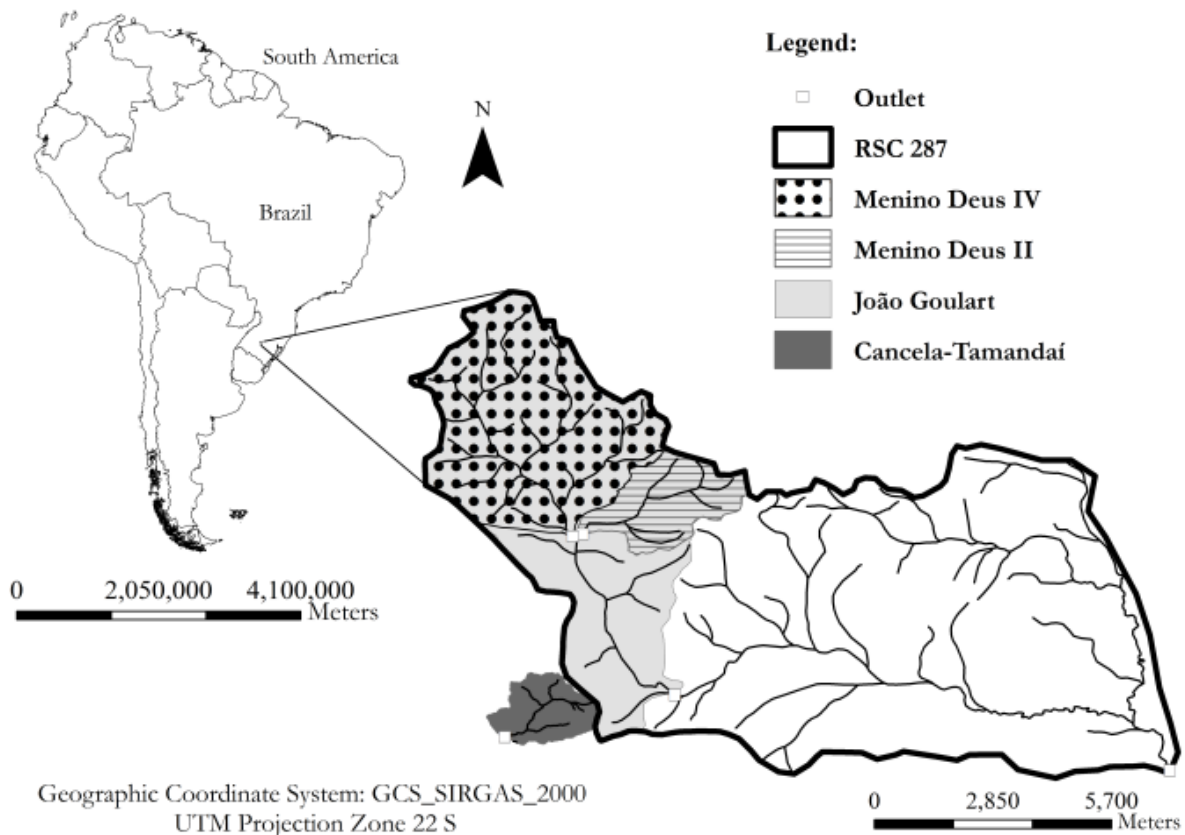
with  $t_{min}$  being the time in which the MDOD occurs,  $f$  is the photoperiod duration (hours), and  $\eta$  is the correction factor of the photoperiod (dimensionless) given by the equation:

$$\eta = \left( \frac{f}{14} \right)^{0.75} \quad \text{Equation (3)}$$

In order to obtain the analytical solution, the temperature is taken to be constant (Mcbride and Chapra, 2005). The method is indicated for photoperiod between 10 and 14 hours, and  $k_a$  value lower than  $10 \text{ d}^{-1}$ . The photoperiod can be known in advance, but the  $k_a$  is determined by the ADM, justifying the purpose of this work.

### Application of approximate delta method

The study was carried out in five sub-basins in the central region of Rio Grande do Sul (Figure 1). Four sub-basins belong to the Vacacaí Mirim River basin, namely: (i) Menino Deus II, (ii) Menino Deus IV, (iii) João Goulart, and (iv) RSC 287. The fifth sub-basin is Cancela-Tamandaí, belonging to the Vacacaí River basin.



**Figure 1.** Location of the sub-basins.

Source: Authors.

An oximeter brand YSI Model 58 (precision of  $0.1 \text{ mg L}^{-1}$ ) was used to monitor the DO profiles (measured every 15min, except Menino Deus II and IV, where the DO was measured every

20min), while the  $f$  was obtained at the meteorological station of the National Institute of Meteorology – INMET, located in the Federal University of Santa Maria, with approximately 25km of maximum distance between monitoring stations (Graepin, 2016). Fluviometric stations were located in the sub-basin outlet (Figure 1).

#### Menino Deus II sub-basin

Menino Deus II sub-basin has 5.07 km<sup>2</sup>, the second smallest sub-basin under study. This sub-basin is characterized as a headwater basin covered by arboreal vegetation (66%), pasture/crops (19%), urban area (7%), and exposed soil (8%). In the fluviometric station, located on that sub-basin outlet, we determine the DO profile curve by performing 13 field samplings. The average flow rate was 0.37m<sup>3</sup> s<sup>-1</sup>, the average velocity was 0.70m s<sup>-1</sup>, the average depth was 0.24m, the average water temperature ranged from 14.13°C to 22.57°C, and the biochemical oxygen demand (BOD) was 1.7mg L<sup>-1</sup>. We performed only one field sampling to BOD.

The flow rate, depth, and average velocity are important characteristics to explain the values of  $k_a$ , and they were determined through rating curves. The flow rate rating curve used in this work was fitted by Souza and Gastaldini (2014). We fitted the depth and the average velocity rating curves using existing database (Souza; Gastaldini, 2014). Daily water levels were measured by thalimedes equipment (OTT Hydrometrie) in the fluviometric station. The water level was used in rating curves.

However, it was possible to determine the  $k_a$  using the ADM only in two field samplings (Table 1). The  $k_a$  values were 32.4d<sup>-1</sup> and 49.3d<sup>-1</sup>. The impossibility to determine the  $k_a$  has two main reasons: (i) the MDOD occurs before the SN, as shown in Figure 2(a) where the MDOD occurs at 12h10min, while the SN at 13h50min, which makes it impossible to determine  $\Phi$ ; or (ii) the non-formation of an appropriate DO profile, making impossible to obtain the time between MDOD and SN (Figure 2(b)).

Characteristics of this fluviometric station that may influence the determination of  $k_a$  are the turbulence and the water temperature variation (which was higher than 4°C in three field samplings). The presence of stones in the riverbed increases the roughness, combined with low-values of average depth produce a high rate of reaeration coefficient. The water depth, the velocity, and the channel bedside roughness are important to the surface reoxygenation phenomenon, interfering in the process of mass transfer in the air-water interface (Costa *et al.*, 2015). Low depths imply in high rates of reaeration coefficient due to atmospheric reaeration, turning the system unsuitable to apply the method as it is sensitive to small time intervals between MDOD and SN (Chapra, 1997).

**Table 1.** Weather characteristics, hydrodynamic characteristics, and  $k_a$  values in Menino Deus II sub-basin. NC - No curve; MD - MDOD before SN.

Menino Deus II									
Date	Heather characteristics*			Water Temperature (°C)		Hydrodynamic characteristics			$k_a$ (d <sup>-1</sup> )
	Insolation (hours)	Temperature (°C)		Average	Variation	Flow rate (m <sup>3</sup> s <sup>-1</sup> )	Depth (m)	Velocity (m s <sup>-1</sup> )	
		Average	Variation						
12/17/14	0.1	23.84	6.20	19.92	1.10	0.48	0.29	0.84	32.4
01/12/15	9.7	27.96	9.60	21.60	4.70	0.94	0.40	1.15	MD
02/04/15	8.8	26.16	7.40	22.57	2.60	0.56	0.31	0.89	49.3
02/12/15	8.9	26.20	10.40	21.64	6.30	0.49	0.29	0.84	MD
03/12/15	9.1	22.16	11.60	21.14	2.70	0.42	0.27	0.78	NC
03/20/15	8.0	24.56	16.40	21.99	2.60	0.15	0.16	0.48	NC
04/10/15	9.9	19.88	21.60	18.92	2.90	0.46	0.28	0.81	NC
04/24/15	6.5	18.56	10.50	18.16	1.60	0.44	0.27	0.80	NC
05/15/15	4.8	20.32	10.40	17.17	1.80	0.06	0.10	0.31	NC
07/01/15	0.5	12.36	5.80	14.40	2.10	0.15	0.16	0.48	NC
07/15/15	4.9	10.92	5.20	14.13	1.50	0.45	0.28	0.81	NC
08/06/15	7.6	26.16	12.80	17.90	5.10	0.16	0.16	0.49	NC
09/02/15	9.4	15.12	12.20	15.03	2.70	0.07	0.11	0.34	NC

Menino Deus IV									
Date	Weather characteristics*			Water Temperature (°C)		Hydrodynamic characteristics			$k_a$ (d <sup>-1</sup> )
	Insolation (hours)	Temperature (°C)		Average	Variation	Flow rate (m <sup>3</sup> s <sup>-1</sup> )	Depth (m)	Velocity (m s <sup>-1</sup> )	
		Average	Variation						
12/17/14	0.1	23.84	6.20	21.07	1.60	0.05	0.14	0.24	33.6
01/12/15	9.7	27.96	9.60	23.20	6.40	0.61	0.18	0.31	MD
02/04/15	8.8	26.16	7.40	24.70	5.20	0.30	0.14	0.36	MD
02/12/15	8.9	26.20	10.40	23.80	8.30	0.06	0.12	0.11	MD
03/12/15	9.1	22.16	11.60	23.01	4.30	0.04	0.08	0.20	MD
03/20/15	8.0	24.56	16.40	23.90	3.80	0.04	0.09	0.21	MD
04/10/15	9.9	19.88	21.60	19.80	5.30	0.18	0.17	0.19	MD
04/24/15	6.5	18.56	10.50	18.63	2.90	0.21	0.17	0.20	MD
05/26/15	0.0	17.12	3.00	17.50	0.60	0.07	0.08	0.18	174.3
06/19/15	0.5	6.36	5.80	11.40	2.40	0.66	0.18	0.31	MD
07/15/15	4.9	10.92	5.20	13.88	1.90	1.19	0.25	0.68	MD
08/06/15	7.6	26.16	12.80	18.70	6.60	0.26	0.16	0.27	MD
09/02/15	9.4	15.12	12.20	16.20	5.20	0.10	0.09	0.17	MD

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João Goulart									
Date	Weather characteristics*			Water Temperature (°C)		Hydrodynamic characteristics			k <sub>a</sub> (d <sup>-1</sup> )
	Insolation (hours)	Temperature (°C)		Average	Variation	Flow rate (m <sup>3</sup> s <sup>-1</sup> )	Depth (m)	Velocity (m s <sup>-1</sup> )	
		Average	Variation						
12/18/14	12.1	25.32	11.80	23.80	7.30	0.01	0.05	0.04	16.90
01/07/15	0.8	25.96	8.40	24.90	0.60	0.44	0.29	0.28	25.80
01/13/15	11.3	28.92	12.40	29.20	5.70	0.96	0.41	0.42	68.40
02/05/15	10.3	24.80	9.00	25.60	3.00	0.19	0.19	0.18	8.40
03/03/15	8.6	26.72	13.00	25.10	3.10	0.28	0.23	0.22	20.40
03/17/15	9.5	23.12	11.60	24.70	2.50	0.46	0.29	0.28	7.40
03/31/15	9.4	22.00	13.80	21.60	2.90	0.96	0.41	0.42	5.70
04/07/15	9.9	17.20	12.80	19.00	2.30	0.67	0.35	0.35	7.90
04/14/15	3.5	21.64	12.20	21.10	1.50	0.43	0.28	0.27	11.10
04/23/15	2.4	18.64	5.80	19.90	1.90	0.47	0.30	0.29	26.40
05/05/15	9.2	11.48	15.60	14.90	1.60	0.35	0.26	0.24	34.90
05/14/15	5.8	18.60	11.60	17.30	1.40	0.10	0.15	0.13	24.30
06/16/15	9.1	9.32	17.00	12.80	3.40	0.50	0.31	0.30	38.10
07/16/15	0.0	11.92	3.20	14.30	0.70	2.48	0.64	0.70	NC
08/12/15	7.8	23.72	12.60	20.00	2.70	0.01	0.04	0.03	42.60
09/15/15	8.4	22.12	19.80	17.10	3.80	0.06	0.12	0.15	25.00

RSC 287

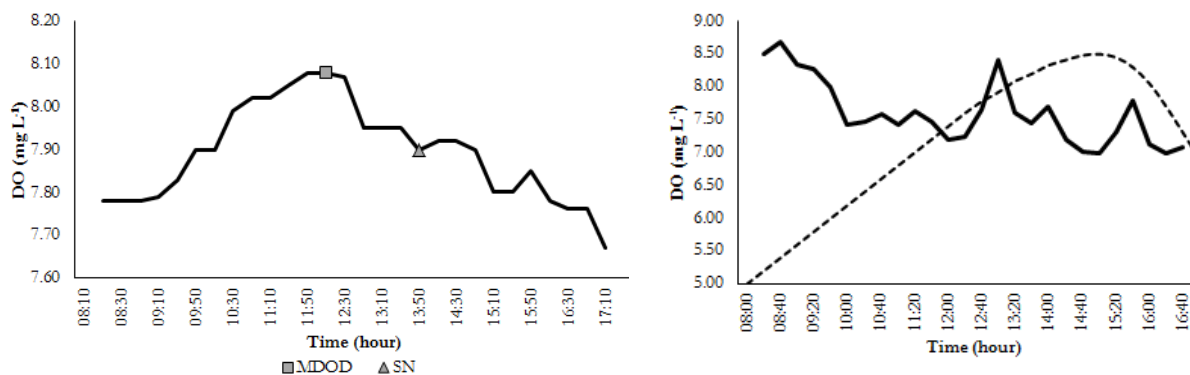
Date	Weather characteristics*			Water Temperature (°C)		Hydrodynamic characteristics			k <sub>a</sub> (d <sup>-1</sup> )
	Insolation (hours)	Temperature (°C)		Average	Variation	Flow rate (m <sup>3</sup> s <sup>-1</sup> )	Depth (m)	Velocity (m s <sup>-1</sup> )	
		Average	Variation						
09/30/15	9.8	16.64	10.80	17.38	4.10	6.4	1.45	0.25	NC
11/06/15	9.7	17.40	11.20	16.26	4.40	17.1	2.75	0.38	NC
12/07/15	11.9	19.68	16.00	21.67	5.20	2.05	0.75	0.10	11.01
12/10/15	11.1	23.72	11.00	22.03	3.30	3.64	1.24	0.10	9.47
01/19/16	5.6	26.4	7.80	21.56	6.80	Zero	-	-	NC
01/21/16	12.1	26.6	10.40	25.95	2.60	Zero	-	-	13.75
02/01/16	10.5	23.52	9.80	24.01	2.60	3.37	0.68	0.13	8.40
05/24/16	4.3	9.84	13.60	11.50	0.80	1.92	1.00	0.13	15.49
06/02/16	7.1	12.32	11.60	13.60	0.50	1.33	0.89	0.10	12.72
06/21/16	5.6	10.60	9.60	10.31	1.00	0.80	0.75	0.08	10.91
07/03/16	8.0	20.80	16.00	12.80	-	2.47	1.02	0.14	NC
07/19/16	8.9	7.28	10.20	10.70	-	1.94	0.96	0.13	NC
08/31/16	3.8	16.12	7.40	16.02	1.10	9.11	-	-	1.18
10/14/16	7.8	21.52	11.00	22.10	2.50	0.8	0.62	0.07	29.16

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conclusion

Cancela-Tamandaí									
Date	Weather characteristics*			Water Temperature (°C)		Hydrodynamic characteristics			k <sub>a</sub> (d <sup>-1</sup> )
	Insolation (hours)	Temperature (°C)		Average	Variation	Flow rate (m <sup>3</sup> s <sup>-1</sup> )	Depth (m)	Velocity (m s <sup>-1</sup> )	
		Average	Variation						
11/04/14	8.4	19.12	6.20	19.84	6.90	0.19	0.23	0.25	NC
12/08/14	6.6	27.24	13.80	23.72	2.60	0.09	0.13	0.21	NC
02/03/15	11.0	26.64	9.60	23.49	4.40	0.14	0.19	0.23	NC
02/26/15	5.3	24.44	12.80	22.96	2.80	0.33	0.33	0.28	NC
03/18/15	8.9	23.08	13.40	22.82	2.50	0.13	0.18	0.23	NC
07/10/15	6.0	16.00	8.80	15.76	1.40	0.15	0.20	0.24	NC
10/23/15	8.3	19.44	7.80	17.73	7.30	0.21	0.25	0.25	NC

\*Source: INMET



(a) Appropriate behavior of DO profile. Minimum DO deficit (MDOD) before solar noon (SN).

(b) No DO profile. Dashed line defines the ideal behavior of the DO profile curve.

**Figure 2.** DO profile in Menino Deus II sub-basin.

Source: Authors.

### Menino Deus IV sub-basin

The Menino Deus IV sub-basin has 19.70 km<sup>2</sup>, and is a headwater sub-basin. Its land cover consists of arboreal vegetation (61%), pasture/crops (26%), exposed soil (7%), and urban area (6%). In the fluvimetric station, located on the sub-basin outlet, we carried out 13 field samplings to determine the k<sub>a</sub>. The field samplings in the sub-basin yielded average flow rate of 0.29m<sup>3</sup> s<sup>-1</sup>, average velocity of 0.26m s<sup>-1</sup>, average depth of 0.14m, average water temperature ranged from



11.40°C to 24.70°C, and BOD of 2.5mg L<sup>-1</sup>. We performed only one field sampling to BOD. The flow was determined by the half-section method, and depth and average velocity by the equations (Santos *et al.*, 2001). The results of the field samplings are shown in Table 1.

In this sub-basin, we were unable to determine the  $k_a$  by the ADM in 11 field samplings. This impossibility was due to the occurrence of MDOD before SN, or by the formation of an inappropriate DO profile curve, similar to the Menino Deus II sub-basin behavior. Water temperature variation was higher than 4°C in seven field samplings.

In only two monitoring field samplings it was possible to determine the values of  $k_a$ . In one of them, the value was 33.6d<sup>-1</sup>, and in the other, the value was 174.3d<sup>-1</sup>. In this case, the oxygen curve profile presented the expected behavior; however, due to the sensitivity of the method to low-values of time between MDOD and SN, which was approximately 0.127hours, there was an overestimation of the  $k_a$ . The occurrence of MDOD before or close to SN is due to a high rate of the reaeration coefficient in the fluvimetric station, caused by the characteristics of the section, similar to Menino Deus II sub-basin. We highlight that in the two cases where the  $k_a$  were calculated, the insolation was close to zero.

In sections with a high rate of reaeration coefficient (higher than 10d<sup>-1</sup>), the method is not efficient (Chapra, 1997), indicating its infeasibility to determine the  $k_a$  in the Menino Deus IV sub-basin.

#### João Goulart sub-basin

The João Goulart sub-basin has 36.17 km<sup>2</sup>, and it is downstream to sub-basins Menino Deus II and IV. The land use and land cover are characterized by arboreal vegetation (61%), pasture/crops (21%), urban area (11%) near the outlet, and exposed soil (7%). To determine the  $k_a$ , flow rate, depth, and average velocity, we performed 16 field samplings in the sub-basin outlet. The average flow rate in the field samplings was 0.52m<sup>3</sup> s<sup>-1</sup>, the average velocity was 0.27m s<sup>-1</sup>, the average depth was 0.27m, and the water average temperature ranged from 12.80°C to 29.20°C. We performed only one field sampling to BOD, indicating 21mg L<sup>-1</sup> or 224.6kg d<sup>-1</sup>. The hydrodynamic characteristics were established by rating curves. The flow rate rating curve was fitted by Teixeira *et al.* (2016). We fitted depth and average velocity rating curve using a previous database (Teixeira *et al.*, 2016). Table 1 shows the values found.

In this sub-basin, it was possible to determine the  $k_a$  using the ADM, once the DO profile curves show an appropriate behavior, except for one field sampling. This field sampling, in particular, occurred in a period of high flow rates, (2.48m<sup>3</sup> s<sup>-1</sup>), approximately 500% higher than the average flow rate of the other field samplings; this could have influenced the non-formation of an adequate DO profile curve.

The values of  $k_a$  ranged between  $5.7d^{-1}$  and  $68.4d^{-1}$ , i.e., an amplitude of  $62.7d^{-1}$ , and average value of  $24.2d^{-1}$ . Variations in the  $k_a$  values for a same fluviometric station are considered normal since the variables that influence the values cannot be totally controlled (Queiroz *et al.*, 2015; Matos; Von Sperling, 2015; Omole *et al.*, 2013; Longe; Musa, 2013). We need to highlight that only at four field samplings the  $k_a$  were less than  $10d^{-1}$ , and in two the water temperature variation was higher than  $4^\circ C$ .

For this fluviometric station, Formentini (2010) proposed an equation using the tracer gas method. The equation by Formentini (2010) was using and most of the values presented differences above 100%. This could be explained by the non-correlation between the  $k_a$ , velocity, and flow (lower than 0.123), input data in Formentini (2010) equation.

#### RSC 287 sub-basin

The RSC 287 sub-basin has  $99.71 \text{ km}^2$ , and it is downstream to the sub-basins Menino Deus II, Menino Deus IV, and João Goulart. The land use and land cover are characterized by arboreal vegetation (46%), pasture/crops (22%), urban area (16%), and exposed soil (16%). To determine the  $k_a$ , flow rate, depth, and average velocity, we conducted 14 field samplings in the fluviometric station, located in the sub-basin outlet. We obtained an average flow rate of  $3.80 \text{ m}^3 \text{ s}^{-1}$ , average velocity of  $0.14 \text{ m s}^{-1}$ , average depth of 1.10m, average water temperature ranged from  $10.31^\circ C$  to  $25.95^\circ C$ , and BOD of  $1.5 \text{ mg L}^{-1}$ . We performed only one field sampling to BOD. The hydrodynamic characteristics were determined by an ADCP (Acoustic Doppler Current Profiler) Sontek RiverSurveyor S5. Table 1 shows the values found.

In this sub-basin, it was possible to determine the  $k_a$  by the ADM in nine out of 14 field samplings. The values of  $k_a$  ranged from  $1.18d^{-1}$  to  $29.16d^{-1}$ , indicating an amplitude of  $27.98d^{-1}$ , and average value of  $13.88d^{-1}$ . The behavior was appropriate of the DO profile curve, with the increase and decrease in DO concentration, being the decline after SN, at 15h30min. However, in some monitoring field samplings, the appropriate profile was not observed, being similar to the DO profile curves of Menino Deus II and IV sub-basins. In four field samplings, the water temperature variation was higher than  $4^\circ C$ , and the formation of an inappropriate profile or unreliable  $k_a$  value could be derived from that. In only three field samplings the  $k_a$  was less than  $10d^{-1}$ .

During the monitoring field samplings, the sub-basin had weather variabilities, which may have contributed to the formation of a non-adequate DO profile curve, as well as its use for irrigation of rice crops. An indicator of these factors is the variability of the hydrodynamic characteristics, such as flow rate, depth, and velocity, which ranged from zero (no flow and velocity, so the equipment does not measure depth) to  $17.10 \text{ m}^3 \text{ s}^{-1}$ , 2.75m, and  $0.38 \text{ m s}^{-1}$ , respectively.

In this sub-basin, it was possible to determine the  $k_a$  by the ADM; however, there are uncertainties in the values due to the behavioral incompatibility of the coefficient with the hydrodynamic characteristics. This agrees with Ávila (2014), which applied the ADM in this sub-basin checking the favorable and uniform values of  $k_a$ ; however, comparing the observed and calculated values through equations from the literature, there were differences between the results.

#### Cancela-Tamandaí sub-basin

The Cancela-Tamandaí sub-basin was the smallest sub-basin studied, with 2.70 km<sup>2</sup>, the only one outside the Vacacaí Mirim River basin. Its land use is composed of urban area (68%), arboreal vegetation (23%), pasture/crops (7%), and exposed soil (2%). To determine the  $k_a$ , flow rate, depth, average velocity and DO profile, seven field samplings were performed in the fluvimetric station, located in the sub-basin outlet. In this sub-basin, we obtained average flow rate of 0.18 m<sup>3</sup> s<sup>-1</sup>, average velocity of 0.24 m s<sup>-1</sup>, average depth of 0.21 m, and average water temperature ranged from 15.76°C to 23.72°C. We performed only one field sampling to BOD with 21 mg L<sup>-1</sup> or 308.4 kg d<sup>-1</sup>. The hydrodynamic characteristics were determined by rating curves. The flow rate rating curve was fitted by Santos and Gastaldini (2016), and we fitted the depth and average velocity rating curve using a database (Santos; Gastaldini, 2016). Table 1 shows the values found.

In this sub-basin, the DO profile curve has not satisfied that of indicated by the method in any of the field samplings, making it impossible to determine the  $k_a$ . In all field samplings, the maximum value of DO occurred early in the morning, with a constant decline of its concentration throughout the photoperiod.

The DO profile curve presented by this sub-basin differs from others most likely because of high values of water BOD (308.4 kg d<sup>-1</sup>), since it has essentially urban characteristics with disposal non-treated domestic effluents (Santos; Gastaldini, 2016). Thus, the constant decline of DO concentration is associated with the presence of liquid effluents with high levels of BOD (Nezlin *et al.*, 2016).

The inefficiency of the ADM in a station with high organic load can be explained by the joint assessment of respiration, photosynthesis, and reaeration effects (McBride; Chapra, 2005). The BOD, associated with water temperature variability (between 1.4°C and 7.3°C), its not feasible the application of the method to the fluvimetric station of the Cancela-Tamandaí sub-basin.

#### **Considerations and conclusions**

In this study, we found the application of the ADM presented limitations in all sub-basins, some of them referred by McBride and Chapra (2005). The limitations observed in this study are related to the following factors: (i) the organic content present in the river section should be regular; (ii)

in rivers with high rates of reaeration coefficient, the MDOD occurred before SN, or presented small values of time between MDOD and SN, causing an overestimation in the values of  $k_a$ ; (iii) the high water temperature variability.

We could not determine the  $k_a$  in 54% of the field samplings. Among the sub-basins studied, João Goulart was the one that allowed a greater number of successes in determining the  $k_a$ . However, when the  $k_a$  was calculated, its values were unreliable due to no correlation with hydrodynamic characteristics, and incompatibility with the equation proposed by Formentini (2010). Then the ADM is not feasibility of applying in urban basin in the central region of Rio Grande do Sul. However, it is important to better explore the limitations of applying the ADM since the method is a low-cost alternative to experimental methods and empirical equations.

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